

3-D CFD ANALYSIS OF HYDROSTATIC BEARINGS

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ABSTRACT

The hydrostatic bearing promises life and speed characteristics currently unachievable with rolling element bearings alone. In order to achieve the speed and life requirements of the next generation of rocket engines, turbopump manufacturers are proposing hydrostatic bearing to be used in place of, or in series with, rolling element bearings.

The design of a hydrostatic bearing is dependent on accurate prediction of the pressure in the bearing. The stiffness and damping of the hydrostatic bearing is very sensitive to the bearing recess pressure ratio. In the conventional approach, usually ad hoc assumptions were made in determining the bearing pressure of this approach is inherently incorrect.

In the present paper, a more elaborate approach to obtain the bearing pressure is used. The bearing pressure and complete flow features of the bearing are directly computed by solving the complete 3-D Navier-Stokes equation .

The code used in the present calculation is a modified version of REACT3D code.

Several calculations has been performed for the hydrostatic bearing designed and tested at Texas A&M. Good agreement has been obtained between computed and test results. Detailed flow features in the bearing will be also described and discussed.

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3-D CFD Analysis of Hydrostatic Bearings

by

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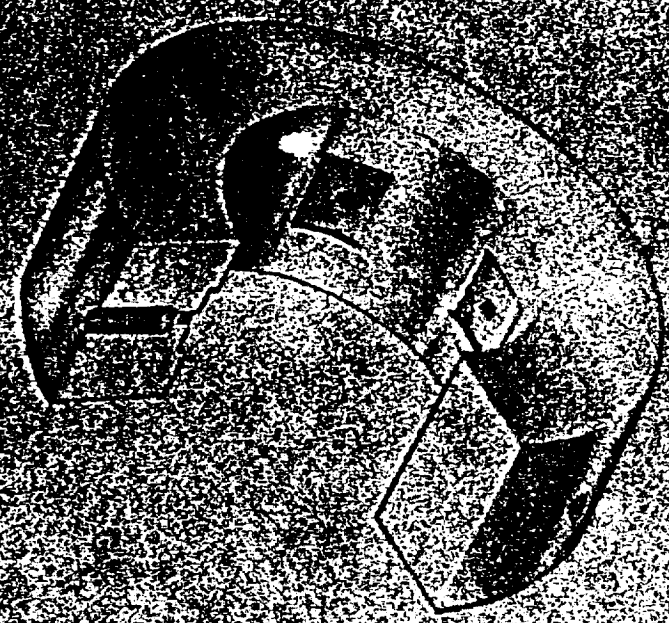
**Benefits of Hydrostatic Bearings in High Power Density
Turbomachinery Led Rocketdyne to Pursue Aggressive IR&D
Initiative to Improve Analysis Capability**

SC89C-31-76

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HYDROSTATIC TEST
(GUTAWAY)

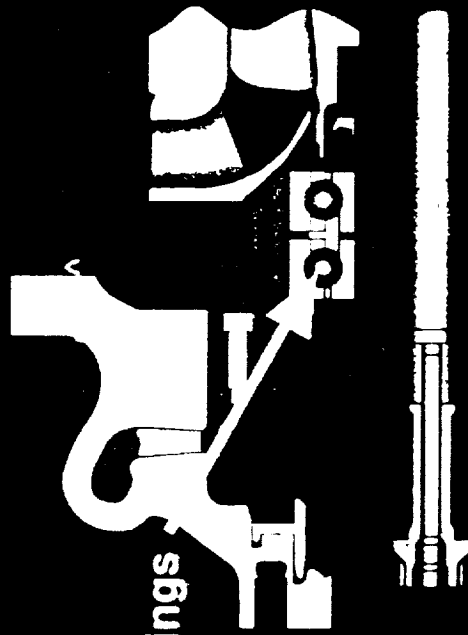


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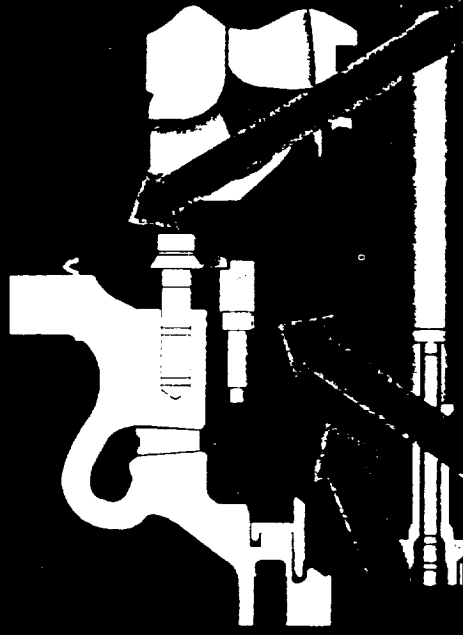
HPOTP Pump End Bearing Conversion

Flight Configuration



Ball Bearings

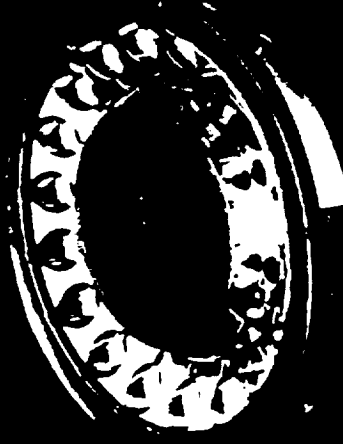
Hydrostatic Bearing Retrofit



Rotor

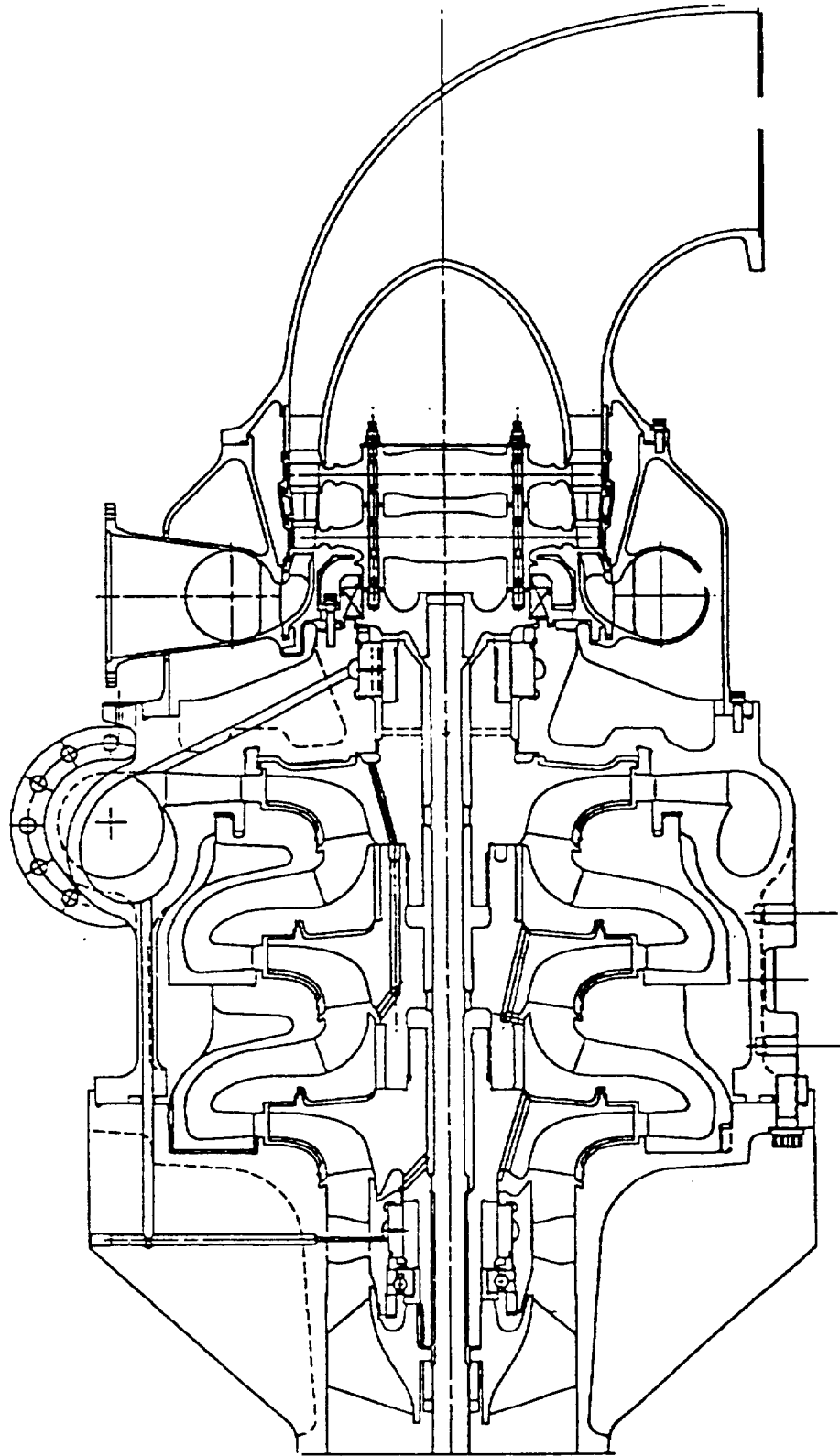


Hydrostatic Bearing



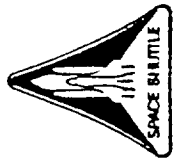
Bearing Support

FUEL PUMP FOR NLS

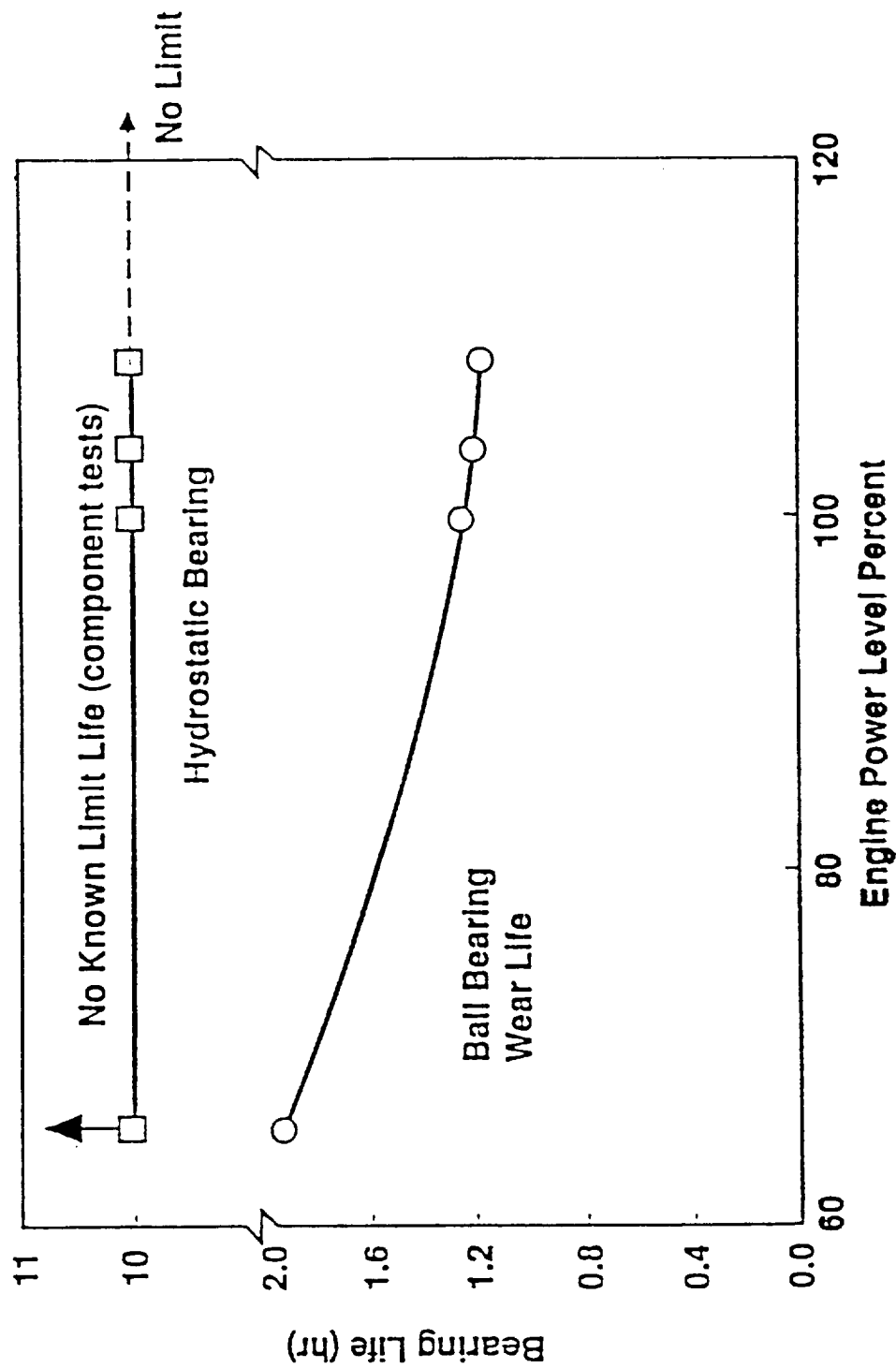


Benefits:

- Low-Wear/ No Known Life Limit
- Reasonable Hardware Cost



Significantly Improved Life & Power Level Margin With Hydrostatic Bearing



920-4-031
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Analysis Requirement:

- Improve Accuracy of Rotordynamic Model Input
 - Direct Stiffness
 - Cross-Coupled Stiffness
 - Direct Damping
 - Added Mass

Analysis Method:

- Bulk-Flow Analysis Operational and Anchored
 - Film-averaged Navier Stokes Eqn Across Lands
 - Recess Pressure Constant / Including orifice
 - Loss Coefficient Used to Determine Pressure at Entrance to Bearing Land
- Currently Improving with Steady-State 3-D CFD
 - Anchor Loss Coefficients for Bulk Flow Model
- Full Bearing Perturbation Solution of 3D Steady-State Solution
- Steady Solution with Eccentric Shaft
- Unsteady Solution with Whirling Shaft



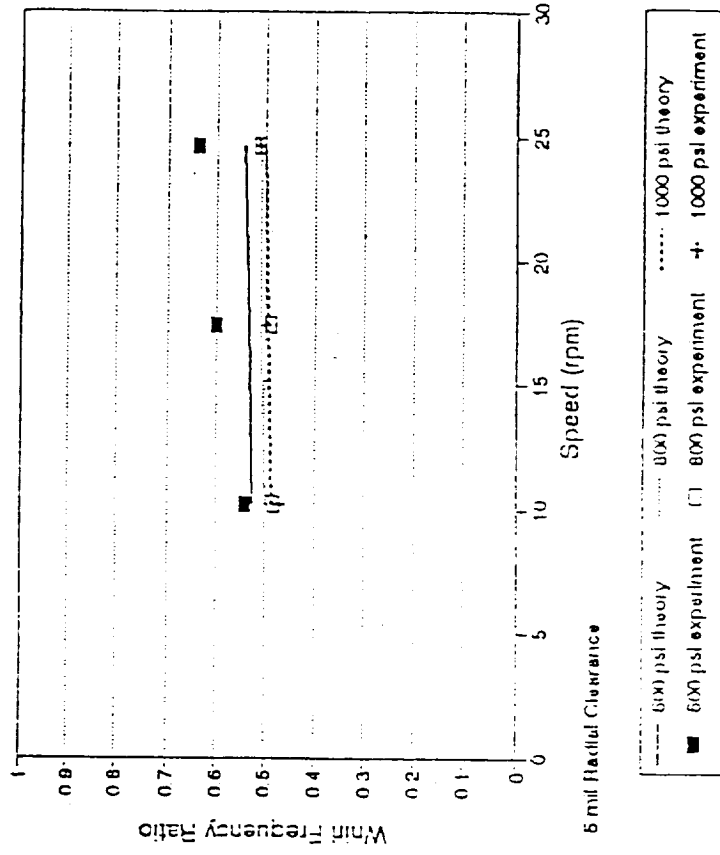
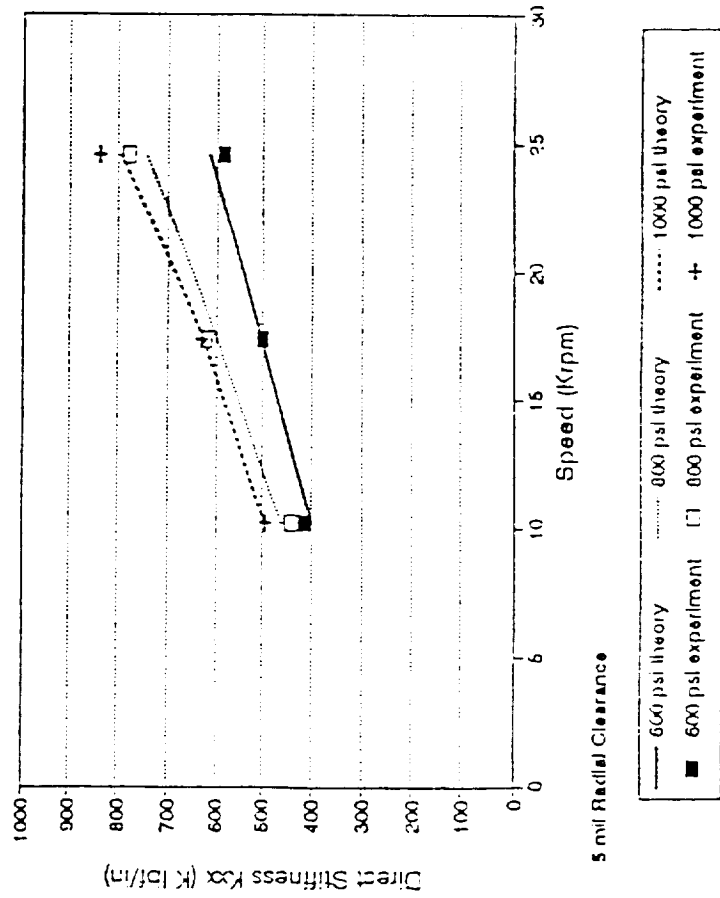
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COMPARISON OF THEORY AND EXPERIMENT

TEXAS A&M HYDROSTATIC BEARING TESTING

Difference

	<u>MIN</u>	<u>AVG</u>	<u>MAX</u>
Direct Stiffness (K_{xx})	-5%	+7%	+20%
Cross-Coupled Stiffness (K_{xy})	-26%	+2%	+16%
Direct Damping (C_{xx})	-22%	-5%	+13%
$WFR = K_{xy} / \omega C_{xx}$ Whirl Frequency Ratio	-15%	+1%	+8%

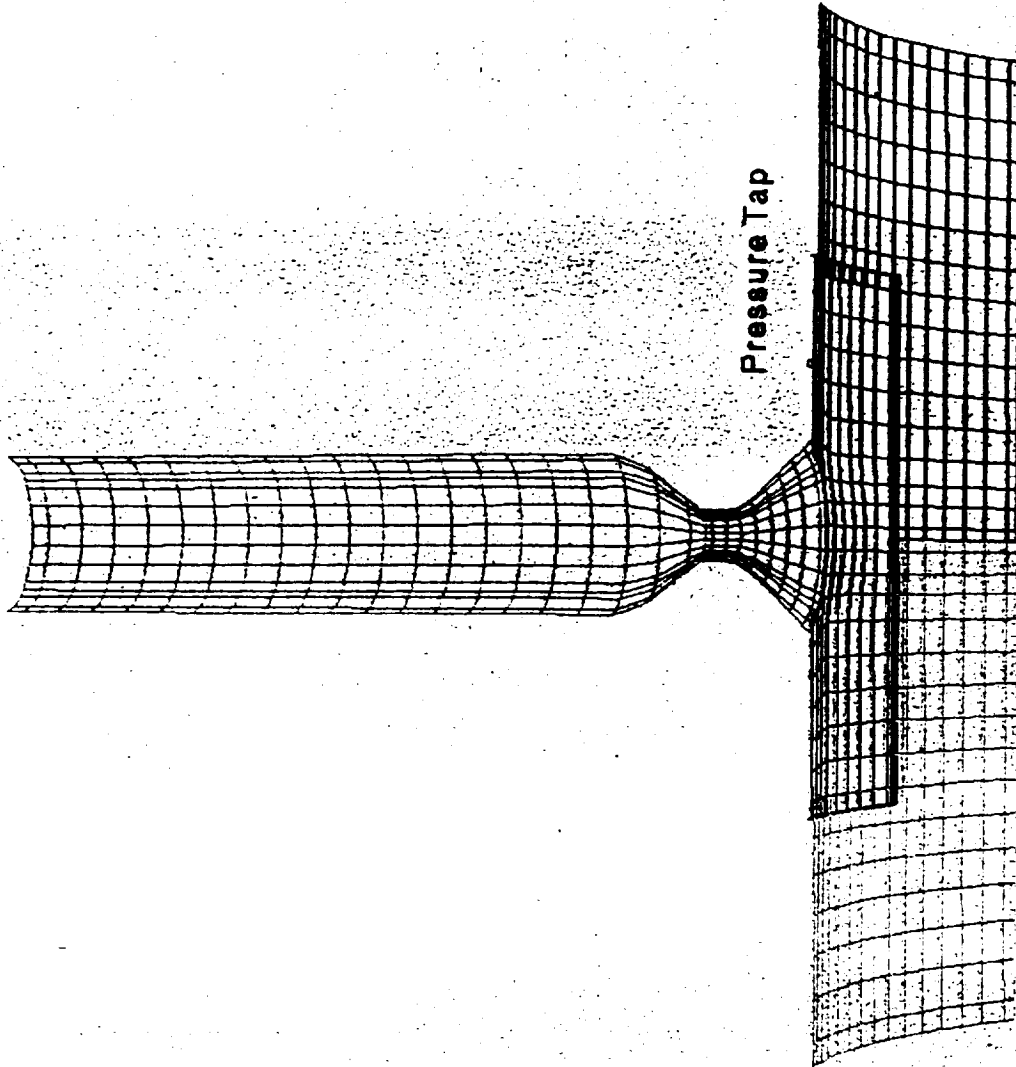


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Grid Generation Challenges:

- Circular Orifice to Square Recess
- Circular Orifice Matching Recess Curvature
- Aspect Ratio in Bearing Land
- Solved Through Multi-Zone Approach
 - 5 Zones Entrance 22X8X8
 Orifice 10X8X8
 Recess 6X20X20
 Land-1 6X32X17
 Land-2 6X32X17
 - Total in Model - 10976

3D Multi-Zone Grid of H/S Bearing



Methodology

- 3 D Steady-State Accurate Finite Volume Formulation in Generalized Coordinates
- Full Navier-Stokes (FNS) 1st and 2nd Order Upwind/Central Spatial Discretization
- Simple Based Velocity-Pressure Coupling
- $k-\varepsilon$ Turbulence Modelling with Wall Function
- Multiple Zone Approach

Boundary Conditions

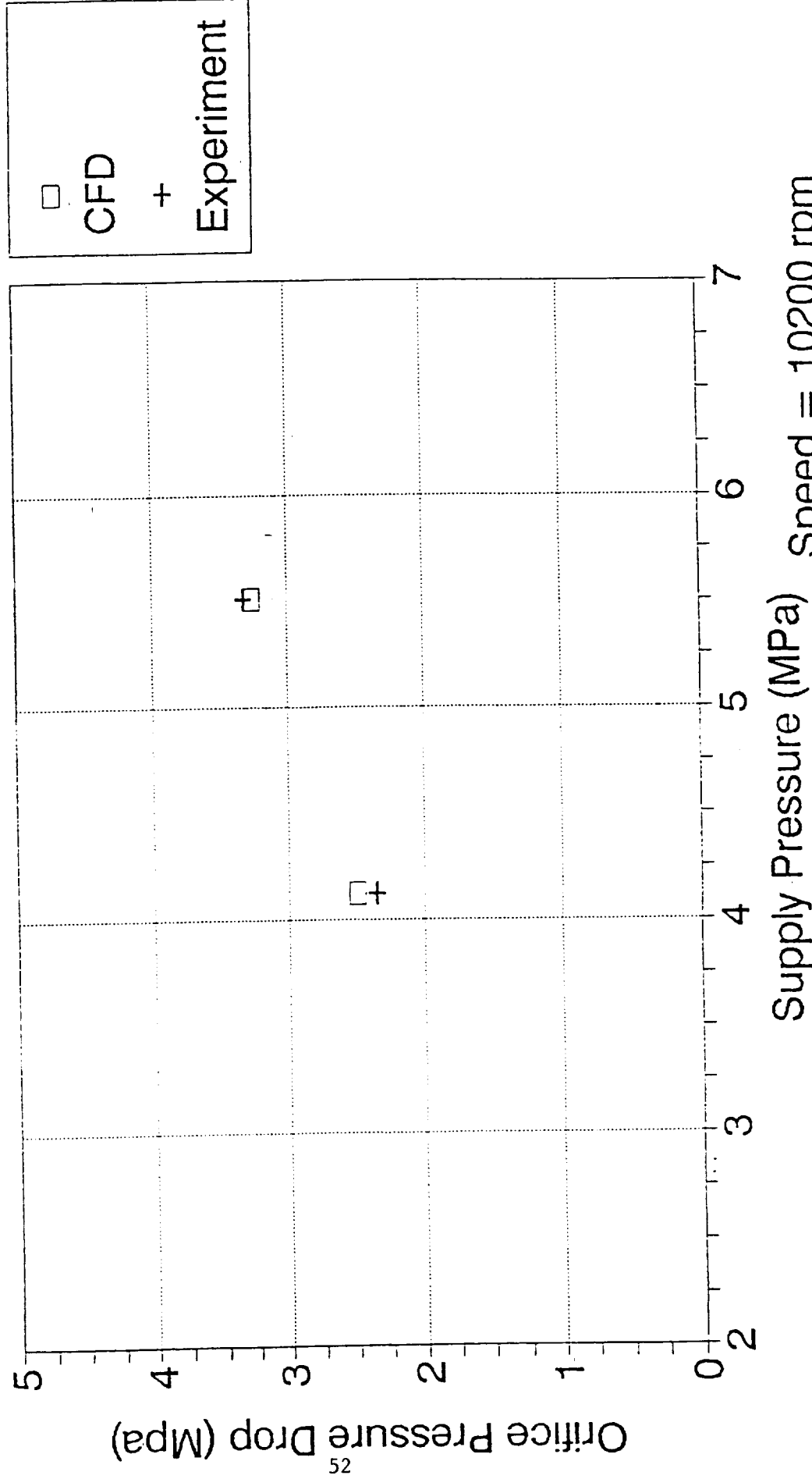
- No-slip at stationary wall
- Specify velocities at the inlet
- Extrapolate the flow velocity variables from the interior point at the outlet
- No slip relative to the rotating shaft
- Periodic conditions between recesses
- Consistent formulation of interface Zonal conditions

Results:

- Within 5% of Recess Pressure Loss
- Qualitative Agreement of Flowfield
- Matches Assumptions of Bulk Flow Model

Code Development and Verification

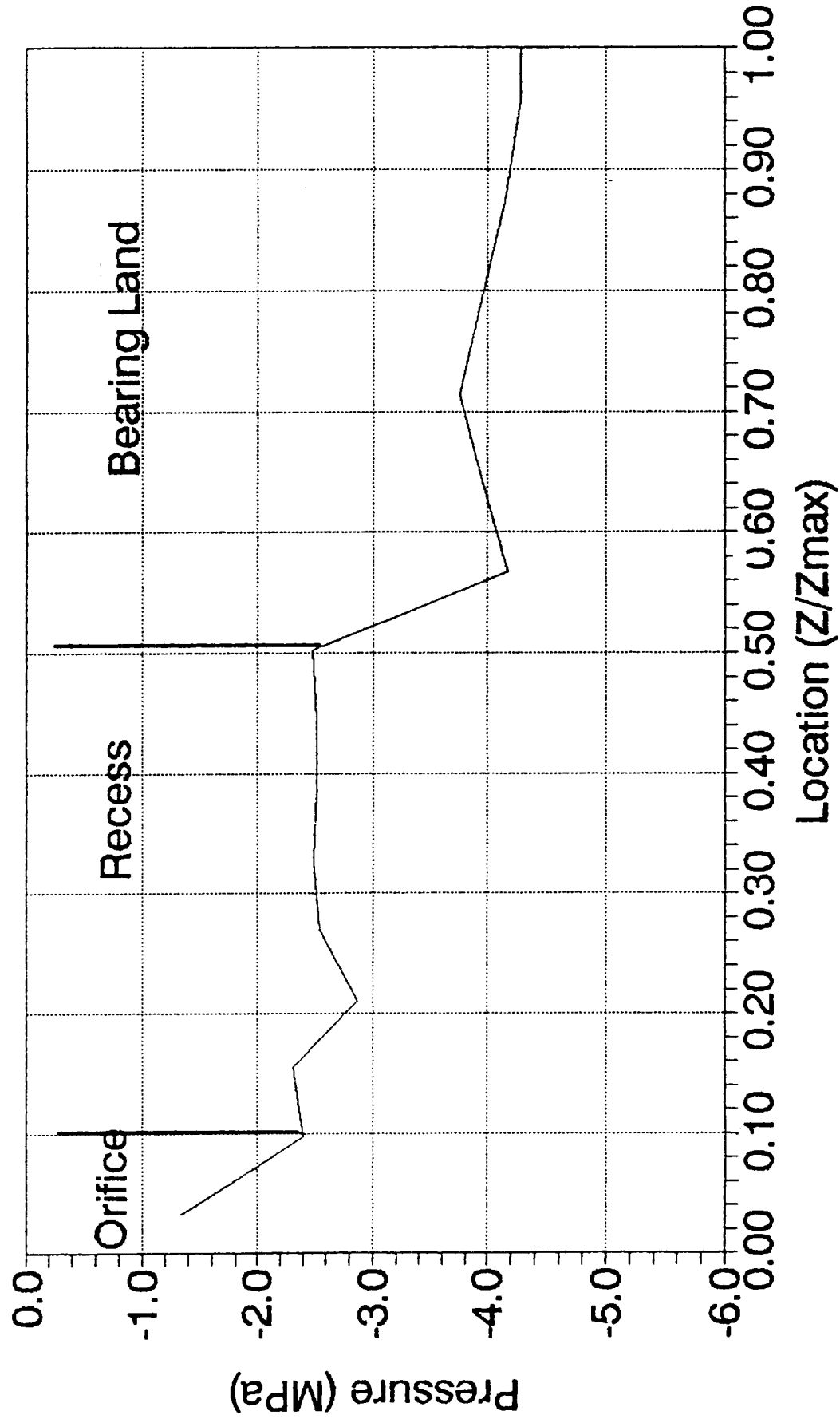
TAMU Data Compared to CFD Solution



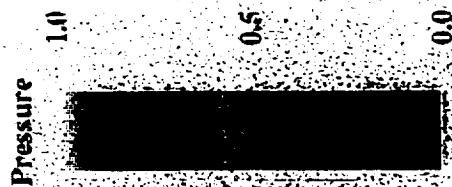
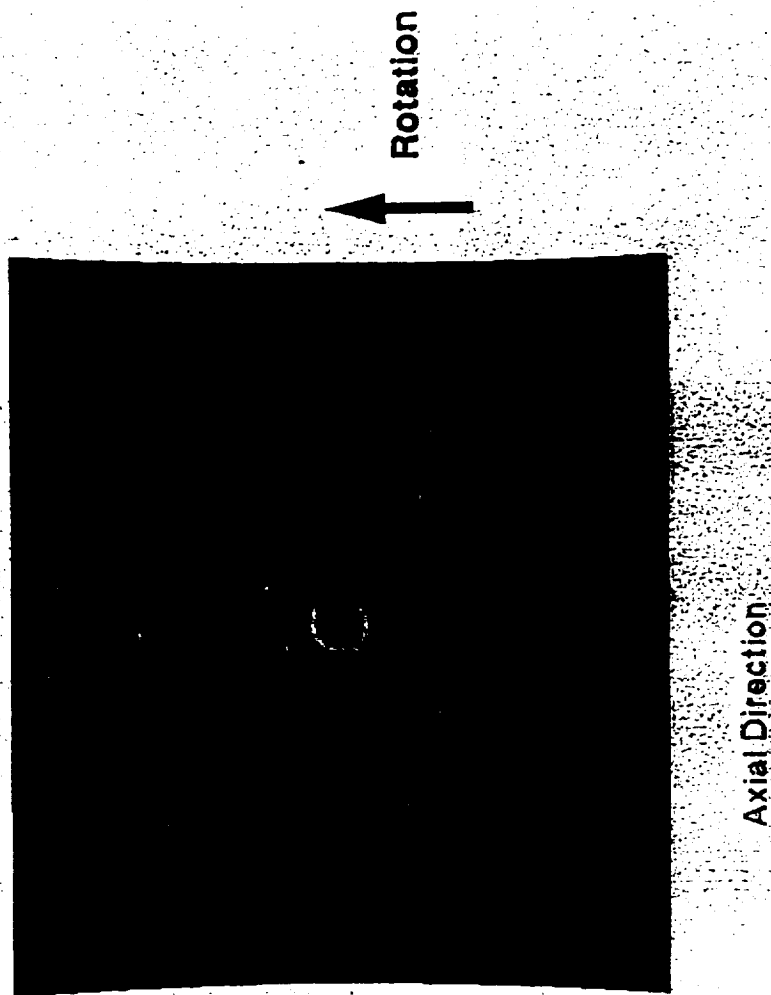
Speed = 10200 rpm
Clearance = 0.126 mm

3-D CFD Pressure Solution

Axial Line Plot in Bearing Clearance



Pressure Contour at Clearance Radial Plane



Conclusions:

- REACT3D Successfully Predicted Hydrostatic Bearing Solution on Actual Concentric Geometry
- 3-D CFD Solution Supports Main Assumptions of Bulk- Flow Model
 - Flow Variables Constant Across Bearing Clearance
 - Recess Pressure Constant
- Improvements to Bulk -Flow Solution will be Determined by Evaluation of Differences
 - Pressure Recovery at Entrance to Recess and Land

